GaN based RF Power Amplifier (Design and Simulation)

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Outline

- RFPA and their key performance metrics
- Why GaN
- Classes of operation
- PA design steps
- Simulation Results



What is an RFPA?



A Power Amplifier (PA) is needed to boost the power before transmission



Some key specifications

$$Gain \qquad G(f) = \frac{P_{out}(f)}{P_{in}(f)}$$

$$Efficiency \qquad \eta = \frac{P_{out}}{P_{DC}}$$

$$Power-aided$$

$$Power-aided$$

$$H_{add} \stackrel{\Delta}{=} \frac{P_{add}}{P_{DC}} = \frac{P_{out} - P_{in}}{P_{DC}}$$

PAE is a more meaningful figure as it subtracts the added RF input power as well.

It is advantageous to operate the PA near saturation to achieve high efficiency.





Some key specifications

Base Station Power Consumption



- RF Power Amplifier and Feeder(60%-80%)
- Power Supply (5%-10%)
- Signal Processing (5%-15%)
- Cooling, Air condition (10%-25%)







Bandwidth is also important



Solid-State PA (SSPA)

Microwave tube-based amplifiers





RF transistor-based amplifiers (SSPA)





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Solid-State PA (SSPA)



Still a choice for very high power applications



Microwave tubes limitations

- Maintenance
- Size
- High voltage



SSPA are replacing the tubes.



- Low Maintenance
- Compact
- Greater reliability



PA power requirement



High voltage and current swings translate into high output power (P= V X I).

In RFPA, complex conjugate matching are not employed at output.



Why GaN

Advantages and disadvantages of GaN device

TABLE 1. Compari	son of device ma	terial properties.			
Material	Band Gap Energy eV	Breakdown E Field MV/cm	Mobility cm²/V/s	Saturated Velocity cm/s	Thermal Conductance W/cm/°K
Gallium nitride	3.4	3.0	1,500	2.7×10^{7}	1.5
Silicon	1.1	0.3	1,300	1.0×10^{7}	1.5
Gallium arsenide	1.4	0.4	6,000	1.3×10^{7}	0.5
Advantag	es:			Low mobility partially offset by high saturation velocity	Disadvantag
High br	eakdown fi	eld enables to b	be used for	high voltage	High cost

- ➤ High current density: high output power with smaller size ➤ Not good linearity compared to GaAs and Si LDMOS
- Outstanding thermal properties with SiC substrate produces \succ Not suitable for low power (but maybe possible in future) Requires harmonic control for high efficiency PA less heat
- > Higher impedance level: more bandwidth and less loss
- High Efficiency: less source (battery) power required \succ



conductivity



PA classifications



General classes

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RFPA structure and design method



Impedance matching network design is the main task



How to find the optimum load



Loadpull: Tune output load to see at what load the Pout and PAE are maximized



How to find the optimum load





Load Pull Measurement setup

Loadpull either using a model in NI AWR/Keysight ADS Or buy dedicated hardware (mechanical setup)



How to find the optimum load





Choose a device and perform a DC simulation to plot ID-VGS

FET Curve T	racer	
Gate	Drain	
DC_FET DC_FET1		
VGS_start=-3.5 VGS_stop=0		
VGS_points=10 VDS_start=28 VDS_stop=28 VDS_points=1	Cree CGH40010F	
	s	
VD0_p0int3=1	CG <u>H</u> 40010F_r6_CGH X1	40_r6
	tcase=25 crth=5.0	

m1 indep(m1)=-2.925 plot_vs(IDS.i, VGS)=0.100 DC_FET1.VDS=28.000



Subsequently, we stabilize the device.



Perform a fundamental loadpul simulation



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Choose an optimum load impedance





Design the matching networks

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	. <u>*</u> _v	DC Foodt	D.O. SaveAllTrials=no Er=3.68
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			win=50 {t}.{-o} lin=162.6 {t}.{-o w6=83.8262 {t
MLIN C2 TL19 C2	MTAPER Taper1	MLIN TL23	win=50 {t}.{-o} lin=162.6 {t}.{-o} w6=83.8262 {t l6=53.0119 {-6
MLIN C TL19 C2 Subst="M Sub1" C=100 pF	MTAPER Taper1 Subst="MSub1"	MLIN TL23 Subst="MSuu"" Xum=2 7=8.7.1*19 Obm	win=50 {t}.{-o} lin=162.6 {b} {-o w6=83.8262 {-t l8=53.81019 {-b w2=62:1532 {b}
MLIN C TL19 C2 Subst="MSub1" C=100 pF W=84 mil	MTAPER Taper1 Subst=7MSub1" W1=64 mit	MLIN TL23 Subst="MSup" W=150 mit	win=50 {t}.{-o} [in=162.6 {t} {-o} w6=83.8262 {-t} l6=53.0119 {-b} w2=62:1532 {b} [2=433.265 {o}]
MLIN C TLI9 C2 TLI9 C2 Subst="MSub1" C=100 pF W=84 mil TermG L=100 mil	MTAPER Taper1 Subst="MSub"1" W1=64 mit W2=150 mil	MLIN TL23 Subst="MSub" W=150 mil MLIN L=20 mil	win=50 {t}.{-o} lin=162.6 {θ {-o w6=83.8262 {-t l6=53.0119 {-6 w2=62.1532 {e} l2=433.265 {o} l1=169.277 {o}
MLIN C TL19 C2 Subst="MSub1" C=100 pF W=64 mil L=100 mil TermG1	MTAPER Taper1 Subst="M Sub1" W1=84 mi1 W2=150 mi1 L=40 mi1	MLIN TL23 Subst="MSuu"" W=150 mil TermG2 Num=2 Z=8.7-j*19 Ohm MLIN L=20 mil	win=50 {t}.{-o} lin=162.6 {t}.{-o} w6=83.8262 {-t} l6=53.0119 {-t} w2=62:1592 {b} l2=433.265 {o} l1=169.277 {a} w3=58.8378 {o}
MLIN C TL19 C2 Subst="MSub1" C=100 pF W=64 mil TermG TermG Num=1	MTAPER Taper1 Subst="M Sub1" W1=84 mi1 W2=150 mi1 L=40 mi1	MLIN TL23 Subst="MSuu" W=150 mil TL22 Subst="MS ub1" TL22 Subst="MS ub1"	win=50 {t}.{-o} lin=162.6 {t}.{-o} w0=83.8262 {-t l8=53.0119 {-t} w2=62:1532 {o} l2=433.265 {o} l1=169.277 {a} w3=58.8378 {o} l3=387.856 {o}
MLIN C TL19 C2 Subst="MSub1" C=100 pF W=64 mil L=100 mil TermG TermG TermG Z=50 Ohm	MTAPER Taper1 Subst="MSub1" W1=84 mi1 W2=150 mi1 L=40 mi1	MLIN TL23 Subst="MSub" W=150 mil TermG2 Num=2 Z=8.7-j*19 Ohm MLIN L=20 mil TL22 Subst="MSub1" W=win mil	win=50 {t}.{-o} lin=162,6 {₿ {-o} w6=83.8262 {-t} l8=53.0119 {-b} w2=62:1532 {o} l2=433.266 {o} l1=169.277 {o} w3=58.8378 {o} l3=387.856 {o} w4=18:5421 {o} w4=18:5
MLIN C TL19 C2 Subist="MSub1" C=100 pF W=84 mil TermG TermG1 Num=1 Z=50 Ohm	MTAPER Taper1 Subis="MSub1" W1=64 mi1 W2=150 mi1 L=40 mi1	MLIN TL23 Subst="MSub" W=150 mil TL22 Z=8.7-j*19 Ohm MLIN L=20 mil TL22 Subst="MSub1" W=win mil	win=50 {t}.{-o} lin=162.6 {B {-o} w6=83.8262 {-t} l8=53.0119 {-b} w2=62:1532 {o} l2=433.265 {o} l1=169.277 {a} w3=58.8378 {o} i3=387.856 {o} i4=617.014 {o} i4=617.014 {o}
MLIN C TL19 C2 TL19 C2 Subst="MSub1" C=100 pF W=84 mil TermG L=100 mil TermG1 Num=1 Z=50 Qhm	MTAPER Taper1 Subst='MSub1'' W1=64 mi1 W2=150 mi1 L=40 mi1	MLIN TL23 Subst="MSub" W=150 mil TL22 Z=8.7-j*19 Ohm. MLIN L=20 mil TL22 Subst="MSub1" W=win mil L=lin mil	win=50 {t}.{-o} lin=162.6 {8 {-o} w6=83.8262 {-t} l8=53.0119 {-b} w2=62:1532 {b} l2=433.265 {o} l1=169.277 {a} w3=58.8378 {o} i3=387.856 {o} i4=617.014 {o} w5=140.662 {b}
MLIN C TL19 C2 Subst="MSub1" C=100 pF W=84 mil TermG L=100 mil TermG1 Num=1 Z=50 Ohm	MTAPER Taper1 Subst="M Sub"1" W1=64 mi1 W2=150 mi1 L=40 mi1	MLIN TL23 Subst="MSub" W=150 mil TL22 W=150 mil TL22 Subst="MSub1" W=win mil L=lin mil	win=50 {t}.{-o} lin=162.6 {8 {-o} w6=83.8262 {-t} l8=53.0119 {-b} w2=62:1582 {b} l2=433.265 {o} l1=169.277 {a} w3=58.8378 {b} i3=387.856 {o} i4=817.014 {o} i4=617.014 {o} i5=573.993 {a}
MLIN C TL19 C2 Subst="MSub1" C=100 pF W=64 mil L=100 mil TermG1 Z=50 Qhm	MTAPER Taper1 Subst="MSub1" W1=84 mi1 W2=150 mi1 L=40 mi1	MLIN TL23 Subst="MSuu" W=150 mil MLIN L=20 mil TermG2 Num=2 Z=8.7-j*19 Ohm MLIN W=150 mil TL22 Subst="MSub1" W=win mil L=lin mil	win=50 {t}.{-o} lin=162.6 {b} {-o} w6=83.8262 {-t} l8=53.0119 {-b} w2=62:1532 {b} l2=433.266 {o} l1=169.277 {a} w4=58.8378 {b} i3=387.856 {o} i4=817.014 {o} w5=140.662 {b} l5=573.993 {o}
MLIN C TL19 C2 Subst="MSub1" C=100 pF W=64 mil L=100 mil TermG1 Num=1 Z=50 Ohm	MTAPER Taper1 Subist="MSubi1" W1=64 mi1 W2=150 mi1 L=40 mi1	MLIN TL23 Subst="MSubit" W=150 mil TermG2 Num=2 Z=8.7-j*19 Ohm MLIN L=20 mil V=win mil L=lin mil	win=50 {t}.{-o} lin=162.6 {B {-o} w0=83.8262 {-t} l0=53.0119 {-b} w2=62.1532 {o} l2=433.265 {o} l1=169.277 {a} w3=58.8378 {o} i3=387.856 {o} i4=817.014 {o} w5=140.662 {o} j5=573.993 {o}
MLIN C TL19 C2 Subist="MSub1" C=100 pF W=84 mil TermG TermG1 Num=1 Z=50 Ohm	MTAPER Taper1 Subst='MSub1" W1=64 mi1 W2=150 mi1 L=40 mi1	MLIN TL23 Subst="MSub1" W=150 mil TL22 Subst="MSub1" W=win mil L=lin mil	win=50 {t}.{-o} lin=162.6 {B {-o} w6=83.8262 {-t} l8=53.0119 {-b} w2=62:1532 {o} l2=433.265 {o} l1=169.277 {a} w3=58.8378 {o} i3=387.856 {o} i4=617.014 {o} w5=140.662 {o} l5=573.993 {o}
MLIN C TLI9 C2 TLI9 C2 Subst="MSub1" C=100 pF W=84 mil TermG L=100 mil TermG1 Num=1 Z=50 Qhm	MTAPER Taper1 Subist='MSub1'' W1=64 mi1 W2=150 mi1 L=40 mi1	MLIN TL23 Subst="MSub" W=150 mil TL22 VW=150 mil TL22 Subst="MSub1" W=win mil L=lin mil	win=50 {t}.{-o} lin=162.6 {8 {-o} w6=83.8262 {-t} l8=53.0119 {-b} w2=62:1532 {b} l2=433.265 {o} l1=169.277 {a} w3=58.8378 {o} i3=387.856 {o} i4=617.014 {o} w5=140.662 {o} l5=573.993 {o}
MLIN C TL19 C2 Subst="MSub1" C=100 pF W=64 mil TermG1 Z=50 Qhm Z=50 Qhm	MTAPER Taper1 Subst="MSub1" W1=84 mi1 W2=150 mi1 L=40 mi1	MLIN TerinG TL23 Subst="MSub" Subst="MSub" Num=2 W=150 mil Z=8.7-j*19 Ohm. MLIN L=20 mil TL22 Subst="MSub" Subst="MSub" W=win mil L=lin mil GO/AL'	win=50 {t}.{-o} lin=162.8 {b} {-o} w6=83.8262 {t} l8=53.0119 {-b} w2=62:1532 {o} l2=433.266 {o} l1=169.277 {a} w3=58.8378 {o} i3=387.856 {o} i4=817.014 {o} w5=573.993 {o}
MLIN C TL19 C2 Subst="MSub1" C=100 pF W=64 mil L=100 mil TermG1 Num=1 Z=50 Ohm S-PARAMETERS,	MTAPER Taper1 Subst="MSub1" W1=84 mi1 W2=150 mi1 L=40 mi1	MLIN TL23 Subst="MSubit" W=150 mil TermG2 Num=2 Z=8.7-j*19 Ohm MLIN L=20 mil TL22 Subst="MSub1" W=win mil L= lin mil GOAL'	win=50 {t}.{-o} lin=162.6 {b} {-o} w0=83.8262 {-t} l8=53.0119 {-b} w2=62:1532 {o} l2=433.265 {o} l1=169.277 {a} w4=58.8378 {o} i3=387.858 {o} i4=817.014 {o} w5=140.662 {o} l5=573.993 {o}
MLIN C TL19 C2 Subis="MSub1" C=100 pF W=64 mil TermG TermG1 Num=1 Z=50 Ohm S-PARAMETERS	MTAPER Taper1 Subist="MSubi1" W1=64 mi1 W2=150 mi1 L=40 mi1	MLIN TL23 Subst="MSubit" W=150 mil TermG2 Num=2 Z=8.7-j"19 Ohm MLIN L=20 mil W=win mil L= lin mil GOAL Goal	win=50 {t}.{-o} lin=162.6 {B {-o} w0=83.8262 {-t} l0=53.0119 {-b} w2=62.1532 {o} l2=433.265 {o} l1=169.277 {a} w3=58.8378 {o} i3=387.856 {o} i4=817.014 {o} w5=140.662 {o} l5=573.993 {o}
MLIN C TL19 C2 Subist="MSub1" C=100 pF W=84 mil TermG TermG TermG1 Num=1 Z=50 Qhm S-RARAMETERS S_Param	MTAPER Taper1 Subist='MSub1" W1=64 mi1 W2=150 mi1 L=40 mi1	MLIN TL23 Subst="MSubit TerinG Term02 Num=2 Z=8.7-j*19 Ohm MLIN L=20 mil L Subst="MSub1" Z=8.7-j*19 Ohm W=150 mil Z=8.7-j*19 Ohm TL22 Subst="MSub1" Subst="MSub1" Z=8.7-j*19 Ohm W=win mil L Goal OptimGoal 1	win=50 {t}.{-o} lin=162.6 {B {-o} w6=83.8262 {-t} l8=53.0119 {-b} w2=62.1532 {o} l2=433.265 {o} l1=169.277 {a} w3=58.8378 {o} i3=387.856 {o} i4=617.014 {o} w5=140.662 {o} l5=573.993 {o}
MLIN C TL19 C2 Subst="MSub1" C=100 pF W=64 mil TermG1 Z=50 Qhm S-PARAMETERS S_Param SP1	MTAPER Taper1 Subst="MSub1" W1=84 mi1 W2=150 mi1 L=40 mi1	MLIN TL23 Subst="MSubit" W=150 mil MLIN L=20 mil TerinG Num=2 Z=8.7-j*19 Ohm W=win mil L=lin mil GO/AL Goal OptimGoal1 Expr="real(Yin1)"	win=50 {t}.{-o} lin=162.6 {€ {-o} w6=83.8202 {t}. l8=53.0119 {-b} w2=62:1532 {o} l2=433.205 {o} l1=169.277 {o} w3=58.8378 {o} i3=387.856 {o} i4=817.014 {o} w5=573.993 {o}
MLIN C TL19 C2 Subst="MSub1" C=100 pF W=64 mil L=100 mil TermG1 Num=1 Z=50 Ohm S RARAMETERS S_Param SP1 Start=1 GHz	MTAPER Taper1 Subst="MSub1" W1=84 mi1 W2=150 mi1 L=40 mi1	MLIN TL23 Subst="MSubit" W=150 mil TermG2 Num=2 Z=8.7-j*10 Ohm MLIN L=20 mil TL22 Subst="MSub1" W=win mil L=lin mil GOAL Goal OptimGoal1 Expr="real(Yin1)" SimInstanceName="SP1"	win=50 {t}.{-o} lin=162.8 {b} {-o} w0=83.8262 {-t} l0=53.0119 {-b} w2=62:1532 {o} l2=433.266 {o} l1=169.277 {a} w3=58.8378 {b} i3=387.858 {o} i4=817:014 {o} w5=140.662 {o} l5=573.993 {o}
MLIN C TL19 C2 Subst="MSub1" C=100 pF W=64 mil L=100 mil TermG TermG1 Num=1 Z=50 Ohm S-RARAMETERS S_Param SP1 Start=1 GHz Stop=3 GHz	MTAPER Taper1 Subst="MSub1" W1=84 mi1 W2=150 mi1 L=40 mi1	GOAL GOAL Goal OptimGoal1 Expr="real(Yin1)" Weight=1	win=50 {t}.{-o} lin=162.6 {b} {-o} w0=83.8262 {-t} l0=53.0119 {-b} w2=62:1532 {o} l2=433.265 {o} l1=169.277 {a} w4=58.8378 {o} i3=387.856 {o} i4=817.014 {o} w5=140.662 {o} (5=573.993 {o})
MLIN C TL19 C2 Subist="MSub1" C=100 pF W=64 mil TermG TermG1 Num=1 Z=50 Ohm S-PARAMETERS S_Param SP1 Start=1 CHz Stop=3 GHz Step=25 MHz	MTAPER Taper1 Subist="MSubi1" W1=64 mi1 W2=150 mi1 L=40 mi1	MLIN TL23 Subst="MSubit" W=150 mil TL22 Subst="MSubit" W=win mil L=lin mil GOAL Goal OptimGoal1 Expr="real(Yin1)" SimInstanceName="SP1"	win=50 {t}.{-o} lin=162.6 {B {-o} w0=83.8262 {-t} 8=53.0119 {-b} w2=62.1532 {o} 12=433.265 {o} 11=169.277 {a} w3=58.8378 {o} i3=387.856 {o} i4=817.014 {o} w5=140.662 {o} (5=573.993 {o} 15=573.993 {o} 15=575.995 {o} 15=575.995 {o} 15=575.995 {o} 15=575.99



Perform EM simulation/optimize





Final optimized design





Simulated results of Final PA: Power sweep





Simulated results of Final PA: Frequency Sweep





Final optimized design







Conclusion

RFPA design employing a GaN device is a very current topic

RFPA design involves a great deal of time on simulation, a good device model and an EDA tool are quite helpful.

One needs to perform a number of simulations and optimization at different level.

Our RFPA design using a Wolfspeed 10W GaN device shows an excellent performance in simulation.

The measurement results of prototype will be shared once the measurements are complete.

If you have any questions or would like to collaborate with me, please feel free to drop me an email at <u>mohammad.maktoomi@scranton.edu</u>.



References

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(2) P. Colantonio, F. Giannini and E. Limiti, High Efficiency RF and Microwave Solid State Power Amplifiers, New York:Wiley, 2009

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